Crossover between two different magnetization reversal modes in arrays of iron oxide nanotubes

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The magnetization reversal in ordered arrays of iron oxide nanotubes of 50 nm outer diameter grown by atomic layer deposition is investigated theoretically as a function of the tube wall thickness d_w. In thin tubes \(d_w<13\) nm the reversal of magnetization is achieved by the propagation of a vortex domain boundary, while in thick tubes \(d_w>13\) nm the reversal is driven by the propagation of a transverse domain boundary. Magnetostatic interactions between the tubes are responsible for a decrease in the coercive field in the array. Our calculations are in agreement with recently reported experimental results. We predict that the crossover between the vortex and transverse modes of magnetization reversal is a general phenomenon on the length scale considered.

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I. INTRODUCTION

Magnetic nanoparticles, particles of nanometer size made from magnetic materials, have attracted increasing interest among researchers of various fields due to their promising applications in hard disk drives, magnetic random access memory, and other spintronic devices.1–5 In addition, these magnetic nanoparticles can be used for potential biomedical applications, such as magnetic resonance imaging (the nanoparticles can be used to trace bioanalytes in the body), cell and DNA separation, and drug delivery.6 To apply nanoparticles in various potential devices and architectures, it is very important to control the size and shape and to keep the thermal and chemical stability of the nanoparticles.7

The properties of virtually all magnetic materials are controlled by domains—extended regions where the spins of individual electrons are tightly locked together and point in the same direction. Where two domains meet, a domain wall forms. Measurements on elongated magnetic nanostructures8 highlighted the importance of nucleation and propagation of a magnetic boundary, or domain wall, between opposing magnetic domains in the magnetization reversal process. Domain-wall propagation in confined structures is of basic interest.9,10 For instance, by equating the direction of a domain’s magnetization with a binary 0 or 1, a domain wall also becomes a mobile edge between data bits: the pseudo-one-dimensional structure can thus be thought of as a physical means of transporting information in magnetic form. This is an appealing development because computers currently record information onto their hard disks in magnetic form.11

The truesphere remains the preferred shape for nanoparticles but this geometry leaves only one surface for modification, complicating the generation of multifunctional particles. Thus, a technology that could modify differentially the inner and outer surfaces would be highly desirable.12 On one hand, over the past years there has been a surge in research on nanocrystals with core/shell architectures. Although extensive studies have been conducted on the preparation of core/shell-structured nanoparticles, the fabrication and characterization of bimetallic core/shell particles with a total size of less than 10 nm and with a monolayer metal shell remain challenging tasks.13 On the other hand, since the discovery of carbon nanotubes by Iijima in 1991,14 intense attention has been paid to hollow tubular nanostructures because of their particular significance for prospective applications. In 2002 Mitchell et al.15 used silica nanotubes offering two easy-to-modify surfaces. More recently, magnetic nanotubes have been grown16–18 that may be suitable for applications in biotechnology, where magnetic nanostructures with low density, which can float in solutions, become much more useful for in vivo applications.12 In this way tiny magnetic tubes could provide an unconventional solution to several research problems and a useful vehicle for imaging and drug delivery applications.

Although the magnetic behavior of nanowires has been intensely investigated, tubes have received less attention, in spite of the additional degree of freedom they present; not only the length L and radius R can be varied, but also the thickness of the wall, d_w. Changes in thickness are expected to strongly affect the mechanism of magnetization reversal, and thereby, the overall magnetic behavior.20,21 However, systematic experimental studies on this aspect were lacking for a long time, mostly due to the difficulty in preparing ordered nanotube samples of very well-defined and tunable geometric parameters.

We recently reported the synthesis and magnetic characterization of a series of Fe_3O_4 nanotube arrays (length L =3 \(\mu\)m, radius \(R=25\) nm, center-to-center distance \(D=105\) nm, and wall thickness 2.5 nm < \(d_w<22\) nm), prepared by atomic layer deposition (ALD) in a porous alumina matrix.22 In this series, the magnetic response of the array, characterized by the coercive field \(H_c\) and the relative remanence,23 varies strongly and nonmonotonically as a function of \(d_w\). For the thinner tubes, \(H_c\) is enhanced by increasing \(d_w\) until \(d_w=13\) nm, at which it presents a maximum of about 780 Oe. For further increases in \(d_w\), the coercive field decreases. A quantitatively similar behavior was also observed in Ni_80Fe_20 nanowire arrays,24 a different system in terms of geometry, material, and preparation techniques.

This convergence of experimental observations may reflect an underlying general phenomenon. Therefore, this pa-
per focuses on the investigation of the nonmonotonic behavior of the coercive field in ferromagnetic nanotube arrays, a question that has remained unexplained until now. We start by modeling the magnetization reversal and calculate $H_c$ for the system reported experimentally,\textsuperscript{22} then generalize our conclusions, and quantitatively predict trends for other geometries and materials.

II. EXPERIMENTAL METHODS

Our approach to the preparation of magnetic nanotubes of well-controlled and tunable geometric parameters and arranged in hexagonally ordered, parallel arrays is based on the combination of two complementary aspects, namely, (i) the utilization of self-ordered anodic alumina (AA) as a porous template and (ii) the conformal coating of its cylindrical pores with thin oxide films by ALD.

Anodic alumina is obtained from the electrochemical oxidation of aluminum metal under high voltage (usually 20–200 V) in aqueous acidic solutions.\textsuperscript{25,26} Under certain proper sets of experimental conditions (nature and concentration of the acid, temperature, and applied voltage), the electrochemically generated layer of alumina displays a self-ordered porous structure. Cylindrical pores of homogeneous diameter are thus obtained, with their long axis perpendicular to the plane of the alumina layer and ordered in a close-packed hexagonal arrangement. With our method, anodization of Al in 0.3M oxalic acid under 40 V at \(8 \degree C\) yields pores of \(\sim 50\) nm outer diameter and with a center-to-center distance of \(\sim 105\) nm (an approach which we will call method A); anodization in 1\% phosphoric acid under 195 V at \(0 \degree C\) yields pores of \(\sim 160\) nm outer diameter and with a center-to-center distance of \(\sim 460\) nm (method B).

Atomic layer deposition is a self-limited gas-solid chemical reaction.\textsuperscript{27} Two thermally stable gaseous precursors are pulsed alternatively into the reaction chamber, whereby direct contact of both precursors in the gas phase is prevented. Because each precursor specifically reacts with chemical functional groups present on the surface of the substrate (as opposed to nonspecific thermal decomposition), one monolayer of precursor adsorbs onto the surface during each pulse despite an excess of it in the gas phase. This peculiarity of ALD makes it suitable for coating substrates of complex geometry (in particular, highly porous ones) conformally and with outstanding thickness control.\textsuperscript{28} We have successfully used ALD to create Fe$_3$O$_4$ nanotubes in porous anodic alumina templates from two different chemical reactions with similar results. In method I, oxidation of ferrocene [also called bis(cyclopentadienyl)lirion, usually abbreviated Cp$_2$Fe] with an ozone/dioxygen (O$_3$/O$_2$) mixture at 200 \(\degree C\) yields a growth rate of \(\sim 0.2\) Å per cycle. Method II consists of the reaction of the dimeric iron(III) tert-butoxide, Fe$_3$(O’Bu)$_2$, with water at 140 \(\degree C\), with \(\sim 0.25\) Å deposited per cycle.\textsuperscript{29} Both methods yield a wall thickness distribution within each sample below 10%.

The results are shown in Figs. 1 and 2. Smooth tubes of 50 or 160 nm outer diameters can be obtained, with aspect ratios on the order of 100. The thickness of the wall can be accurately controlled between 1 and 50 nm. Subsequent re-

![FIG. 1. (Color online) Aspects of Fe$_3$O$_4$ nanotubes grown by (ALD) in a porous anodic alumina matrix. (a) Macroscopic view of the samples, consisting of a circular porous AA membrane containing the embedded tubes, surrounded by an outer circle of Al metal of 2 cm outer diameter; the tubes in the samples from left to right have walls of increasing thickness, approximately 0, 1, 2, 4, 8, 12, and 16 nm (AA obtained according to method A, ALD performed by method I), [(b) and (c)] Scanning electron micrographs (SEMs) of tubes embedded in the porous alumina matrix, observed in top view and at an angle at a break in the sample, respectively; the scale bar represents 200 nm (AA obtained according to method B, ALD performed by method II).](image1)

![FIG. 2. Transmission electron micrographs (TEMs) of isolated tubes from the alumina matrix, with walls of increasing thicknesses, approximately (a) 1, (b) 5, and (c) 13 nm; the scale bar represents 50 nm (AA obtained according to method A, ALD performed by method II).](image2)
structural quality of the tubes is unaffected by reduction,\textsuperscript{22} a consequence of the very small volume contraction caused by it. Our approach allowed us to systematically investigate the influence of structure on magnetism in a series of samples of Fe$_3$O$_4$ nanotube arrays prepared according to methods A and II and in which the wall thickness $d_w$ varies, while all other geometric parameters are maintained constant.

In a series of Fe$_3$O$_4$ nanotube arrays of varying wall thickness $d_w$ (all other geometric parameters being kept constant), investigated by superconducting quantum interference device (SQUID) magnetometry, we observed a significant dependence of the coercivity and remanence on the geometry. In particular, the coercive field $H_c$ can be tuned between 0 and 800 Oe (0 and 80 mT) approximately by properly adjusting $d_w$. Most curiously, the dependence of $H_c$ on $d_w$ is not monotonic—$H_c$ reaches its maximum at $d_w \approx 13$ nm and then decreases for further increases in the wall thickness [Fig. 6(b)]. We interpret this observation as arising from the coexistence of two distinct magnetization reversal modes in our system. Which of the two prevails in a given sample is uniquely determined by the geometric parameters of the tube array. Thus, the cusp in the $H_c(d_w)$ curve corresponds to the crossover between the two modes of magnetization reversal. Section III details the theoretical treatment of the two modes.

III. TWO MAGNETIZATION REVERSAL MODES

For isolated magnetic nanotubes, the magnetization reversal, that is, the change in the magnetization from one of its energy minima ($\mathbf{M}=M_0\mathbf{\hat{z}}$) to the other ($\mathbf{M}=-M_0\mathbf{\hat{z}}$), can occur by one of only two idealized mechanisms, the vortex mode (V), whereby spins in rotation remain tangent to the tube wall, or the transverse mode (T), in which a net magnetization component in the $(x,y)$ plane appears.\textsuperscript{29} In both cases, a domain boundary appears at one end of the tube and propagates toward the other, as illustrated in Fig. 3. Starting from the equations presented by Landeros et al.,\textsuperscript{29} we can calculate the zero-field energy barrier as well as the width of the domain boundary for each reversal mode as a function of the tube thickness $d_w$. Figures 4(a)–4(c) present our results for Fe$_3$O$_4$ nanotubes using $M_0=4.8 \times 10^5$ A/m$^3$ and the stiffness constant $A=10^{-11}$ J/m.\textsuperscript{30} Figure 4(a) shows a crossover at $d_w \approx 20$ nm, showing that the V mode is more stable for thinner tubes, whereas thicker tubes walls favor the T mode.

This result can be qualitatively explained as follow. A very thin tube should behave as a (rolled-up) thin film, in which the magnetic moments always tend to remain within the plane of the film. Conversely, tubes of large wall thicknesses approach the case of wires: surface effects are less crucial, but interactions between diametrically opposed regions become more important.

The presence of a crossover in Fig. 4(a) allows us to expect a transition from the V to the T reversal mode with increasing values of $d_w$. However, the curves cannot give the coercive field values directly because energies represent the difference between a completely saturated state and one with a domain boundary in the middle of the tube. Magnetization reversal, however, is initiated with a domain boundary at one end of the tube, a configuration that corresponds to a lower magnetic energy. From Fig. 4(b) we observe changes in boundary widths between 50 and 120 nm as a function of $d_w$. A crossover is found, corresponding to the one that appears between the energy curves. We shall now proceed to calculate the switching field of an isolated magnetic nanotube assuming that the magnetization reversal is driven by means of one of the two previously presented modes.\textsuperscript{31}

A. Coercive fields

For the T mode, the coercive field $H_c^T$ can be approximated by an adapted Stoner–Wohlfarth model\textsuperscript{32} in which the length of the coherent rotation is replaced by the width of the domain boundary, $w_T$ [see Fig. 4(b)]. Following this approach,

$$H_c^T = \frac{2K(w_T)}{\mu_0 M_0^2}$$

where $K(l) = \frac{1}{2} \mu_0 M_0^2 (1-3N_s(l))$ and $N_s(l)$ corresponds to the demagnetizing factor along $z$, given by $N_s(l) = \frac{2R}{(1-p)^2} \int_0^{\frac{d_w}{2}} [J_1(q) - \beta J_1(q\beta)]^2 (1-e^{-q1/R}),$ with $\beta = 1 - \frac{d_w}{R}$.

For the V mode we use an expression for the nucleation field obtained by Chang et al.\textsuperscript{33} When an external field with magnitude equal to that of the nucleation field is applied opposite to the magnetization of the tube, infinitesimal deviations from the initially saturated state along the tube axis appear. The form of these deviations is determined by the solution of a linearized Brown’s equation.\textsuperscript{34} Furthermore, it has been shown numerically that the solution of this Brown’s equation is not a stable solution to the full nonlinear equation.
at applied fields larger than the nucleation field, and then the only possible stable states are those with uniform alignment along the axis.\textsuperscript{35,36} Thus, the magnetization is assumed to reverse completely at the nucleation field. For an infinite tube, the nucleation field for the V mode, $H_n^V$, is given by

$$\frac{H_n^V}{M_0} = \alpha(\beta) \frac{L^2}{R^2},$$

(2)

with $L_{\text{ex}} = \sqrt{2A/\mu_0 M_0^2}$ and $\alpha(\beta) = q^2$, where $q$ satisfies the condition

$$\frac{qJ_0(q) - J_1(q)}{qY_0(q) - Y_1(q)} = \frac{\beta q J_0(\beta q) - J_1(\beta q)}{\beta q Y_0(\beta q) - Y_1(\beta q)}. \quad (3)$$

Here $J_\alpha(z)$ and $Y_\alpha(z)$ are Bessel functions of the first and second kinds, respectively. Equation (3) has an infinite number of solutions, and the physically correct solution is the smallest one.

Figure 4(c) illustrates the coercive field of an isolated tube with $d_w$ varying from 0.5 to 24.5 nm. We can observe a crossing of the two curves at $d_w = 13$ nm approximately, corresponding to a magnetization reversal for which both the V and T modes mechanisms are possible at the same coercive field. At other given values of $d_w$, the system will reverse its magnetization by whichever mode opens an energetically accessible route first, that is, by the mode that offers the lowest coercivity. Therefore, the curve of coercivity vs $d_w$ is the solid one, and the dotted sections of curves have no physical meaning. Thus, our Fe$_3$O$_4$ tubes will reverse their magnetization by the V mode for $d_w < 13$ nm, and by the T mode for $d_w > 13$ nm. Our calculations for an isolated tube reproduce the nonmonotonic behavior of the coercive field as a function of the wall thickness experimentally observed, with a transition between two different modes causing a cusp at $d_w^{V,T} = 13$ nm (with $d_w^{V,T}$ as the thickness at which the transition occurs). However, the absolute values computed for the coercivity are greater than the experimental data.

B. Effect of the stray field

We ascribe such difference between calculations and experimental results to the interaction of each tube with the stray fields produced by the array—an effective antiferromagnetic coupling between neighboring tubes, which reduces the coercive field [as previously demonstrated in the case of nanowires; see Fig. 6(a)].\textsuperscript{37-40} In these interacting systems, the process of magnetization reversal can be viewed as the overcoming of a single energy barrier $\Delta E$. In an array with all the nanotubes initially magnetized in the same direction, the magnetostatic interaction between neighboring tubes favors the magnetization reversal of some of them. A reversing field aligned opposite to the magnetization direction lowers the energy barrier, thereby increasing the probability of switching. The dependence of the applied field on the energy barrier is often described\textsuperscript{41} by the expression

$$\Delta E = U \left(1 - \frac{H}{H_0}\right)^2,$$

where $H$ is the applied field and $H_0$ denotes the intrinsic coercive field of an isolated wire. For single-domain particles that have a uniaxial shape anisotropy, the energy barrier at
zero applied field, $U$, is just the energy required to switch by coherent rotation, $K(L)$. If we assume that the switching field $H_s$ is equal to $H_c$, then

$$H_s = H'_h - H_{int}, \quad (4)$$

where $H'_h$ denotes the intrinsic coercivity $H'_h$ or $H'_s$ of an isolated tube and $H_{int}$ corresponds to the stray field induced within the array given by

$$H_{int}/M_0 = \frac{2K(L)}{\mu_0 M_0^2} \left( \frac{E_{int}(s)}{K(L)} \right)^{1/2}. \quad (5)$$

In the previous equation we have assumed that the reversal of individual nanotubes produces a decrease in the magnetostatic energy $E_{int}$ that equals the magnetic anisotropy barrier $\Delta E$. Besides, $\varepsilon$ is an adjustable parameter that depends on the distribution of magnetic tubes in space and on the long-distance correlation among the tubes. The value of $\varepsilon$ cannot be obtained from first principles, although values between unity and some tens could be a reasonable estimate for this quantity. Moreover, $E_{int}(s)$ is the magnetostatic interaction between two nanotubes separated by a distance $s$. Such interaction may be calculated by considering each tube homogeneously magnetized and is given by

$$E_{int}(s) = \frac{E_{int}(s)}{V} = \frac{2\mu_0 M_0^2}{(1 - \beta^2) L} \int_0^\infty dq J_0(q) \left( \frac{q}{R} \right)^2 \times \left[ J_1(q) \right]^2 \left(1 - e^{-qL/R} \right).$$

The resulting curve $H_{int}(d_w)$ ($\varepsilon=20$) is illustrated in the top panel of Fig. 6(a). The stray fields produced by an array of nanotubes are significant for the experimentally investigated tubes, being on the order of 350 Oe for $d_w=5$ nm to 580 Oe for $d_w=21$ nm.

C. Results

The hysteresis loop in the normalized axis of a sample of $L=3$ \( \mu \)m, $R=50$ nm, and $d_w=13$ nm is presented in Fig. 5. In this loop we have subtracted the paramagnetic background. Our results are combined in the lower panel of Fig. 6. Experimental data for the coercivity of the array are depicted by dots. In this figure we can observe the strong dependence of the coercivity as a function of the tube wall thickness, evidencing clearly the existence of a maximum. Also, the coercivities of an isolated tube and interacting array obtained from our calculations are depicted in the same figure by dashed and solid lines, respectively. We consider $\varepsilon=20$ in Eq. (4). Note the good agreement between experimental data points and analytical results for interacting arrays for $d_w \geq 8$ nm.

The deviation of the experimental data points from the calculated curve for $d_w \approx 8$ nm likely originates from the structural imperfections of the tubes. Deposition of the magnetic material may lead to granular walls at the initial stages of the growth, whereas further increases in wall thickness accounted a smoothening. Other factors not accounted for in...
our theoretical model include thermal instability, which has a stronger effect in thinner particles, possible shape irregularities, and the finite length of the tubes.

The results presented above may be generalized. We now proceed to investigate how the curve will be affected by changes in the tube radius $R$ and in the material by considering the trajectories of the transition thickness $d_w^{th}$. Such trajectories are shown in Fig. 7 for four different materials. In the range of parameters considered, we observe that an increase in the external radius $R$ results in an increase in the transition thickness $d_w^{th}$. Furthermore, the curves $d_w^{th}(R)$ are steeper for materials with longer exchange lengths. Figure 7 can also be interpreted as a phase diagram, in which each line separates the T mode of magnetization reversal, which prevails in the upper left region of the $(R, d_w)$ space, from the V mode, found in the lower right area.

IV. CONCLUSIONS

In conclusion, by means of simple models for the domain boundary that appears during the magnetization reversal in nanotubes, we can calculate the coercive field in ordered arrays of ferromagnetic nanotubes as a function of the tube wall thickness and the radius. A transition between two different modes of magnetization reversal, from a vortex boundary, in thin tubes, to a transverse boundary, in thick tubes, is responsible for the nonmonotonic behavior of the coercivity as a function of wall thickness experimentally observed. The effect of the stray field originating from the magnetostatic interactions between the tubes of the array must be included to obtain a quantitative agreement between experimental and theoretical results. Because of its long range, the magnetostatic interaction strongly influences the coercivity of the array. Finally, the presence of a coercivity maximum at a certain optimum wall thickness should be a quite general phenomenon, observable for a variety of ferromagnetic materials and of tube radii. Experimental work remains to be done in order to validate these predictions.

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23. That is, the $x$ and $y$ intercepts of the magnetic hysteresis curve, respectively: the remanence is the fraction of the saturated (maximum) magnetization that remains once the applied magnetic field has been turned off, and the coercive field is the absolute value of the magnetic field applied in the $-z$ direction needed to reduce the magnetization in the $+z$ direction to zero (in other words, to erase the remanence).
28 See, for example, B. S. Lim, A. Rahtu, and R. G. Gordon, Nat. Mater. 2, 749 (2003).
31 Strictly speaking, the determination of the coercivity actually requires an analysis of the nonlinear regime, which is lacking at this point. Landeros et al. (Ref. 29) demonstrated that the coherent mode is present only in very short tubes, and that if there is no switching mode other than V and T, results for the nucleation field corresponds to the coercivity.